

In re Application of Carolyn Aita

No.: To be assigned

August 16, 1999

NEW APPLICATION TRANSMITTAL

ELF-REPAIRING CERAMIC COATINGS

Express Mail No. EL294132754US

The Assistant Commissioner for Patents  
 Box Patent Application  
 Washington, D.C. 20231

SIR:

1. Transmitted herewith for filing is the above-identified patent application
2. Enclosed are:
  - ☒ the papers required for a filing date under 37 CFR §1.53(b)
  - \_\_\_\_\_ pages of specification including claims and abstract
  - 1 sheets of drawings ☒ informal \_\_\_\_\_ formal.
  - ☒ Declaration and Power of Attorney (unsigned)
  - \_\_\_\_\_ Assignment with Transmittal (PTO-1595)
  - ☒ Other Specify: return receipt postcard

Applicant is a small entity entitled to a 50% reduction in fees

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Filing Fee Calculations

	Number Filed	Number Extra	Rate	Basic Fee \$760
Total Claims	30 - 20 =	10	x \$18 =	\$180
Independent Claims	6 - 3 =	3	x \$78 =	\$234
_____ Multiple dependent claims if any x \$260 =				\$414

\* If less than zero, enter "0".

Total Filing Fee ..... \$1,174

## 5. Additional Fees

Assignment ..... \$-0-  
 Other Specify ..... \$-0-  
 Total Fees Due \$1,174

## Fee Payment

- ☒ Payment of filing fee deferred
- \_\_\_\_\_ Attached is a check in the amount of \$\_\_\_\_\_ (Filing Fee and Assignment Recordation Fee)
- \_\_\_\_\_ Charge Deposit Account No. 08-1641 in the amount of \$\_\_\_\_\_. A duplicate of this request is attached.
- \_\_\_\_\_ The Commissioner is hereby authorized to charge any additional fees which may be required or credit any overpayment to Deposit Account No. 08-1641, referencing Docket No. \_\_\_\_\_. A duplicate of this request is attached.

By:   
 Edward J. Lynch  
 Registration No. 24,422

Application of

Carolyn Aita

for

UNITED STATES LETTERS PATENT

on

**Self-Repairing Ceramic Coatings**

Drawings: One Sheet

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# **SELF-REPAIRING CERAMIC COATINGS**

## **FIELD OF INVENTION**

The present invention relates to coatings for devices and implements and the like suitable for intracorporeal applications, particularly coatings for  
5 intravascular applications.

## **BACKGROUND OF THE INVENTION**

Biomaterials are synthetic materials used to replace or augment a part of a living system or to function in contact with living tissue. Among the many causes for mortality among human beings, cardiovascular account for  
10 a major portion of such deaths. Therefore, continuous improvements in the development of new and improved biomaterials capable of replacing parts of the cardiovascular system is extremely important. The primary requirements for biomaterials for long-term implants, e.g., heart valve prostheses, stents, and vascular grafts, are biocompatibility, thrombresistivity, nontoxicity, and  
15 durability. Furthermore, biomaterials should be nonirritating to tissue and nondegradable in the harsh physiological environment, neither absorbing blood constituents nor releasing foreign substances into the bloodstream.

A key problem in interfacing a biomaterial with blood revolves around the characteristics of the implant surface. Thrombus and embolism formation at the blood-implant interface is of foremost concern, and is the technology-limiting factor in implant design and materials selection.

5 Metal implants have been used as implants due to their toughness, i.e., the ability to absorb energy before fracture. The metals and metallic alloys commonly used for implants form passivating oxide surface layers at their interface with air. However, the passivation may become destabilized by the acidic (e.g., pH of about 5), saline nature of blood. The surface reactivity of  
10 the metallic implants at the blood-implant interface leads to bulk electrochemical corrosion and localized stress corrosion, which in turn, leads to mechanical failure of the implant and ion contamination of the blood.

Polymer implants or polymer-coated metal implants are commonly used for cardiovascular applications because of their good initial biocompatibility.

15 However, the use of polymers poses a major problem, namely, chemical degradation over time resulting in thrombus and embolism formation as well as the production of harmful wear-related debris.

Ceramic implants offer a compromise by providing chemical inertness, hardness, and wear-resistance. However, ceramic implants exhibit the same

major drawback as that for all traditional bulk ceramic structures in their inability to deform plastically under either or both static and cyclic loading. The lack of flexibility of the bulk ceramics leads to difficulty in manufacturing implants and microcracking during the implant's lifetime in the body due to

5 fatigue failure.

### **SUMMARY OF THE INVENTION**

The present invention is directed to a multilayered protective coating formed of ceramic materials. The coating comprising an inner component or module which has at least two layers of ceramic materials such as zirconia, titania and alumina wherein. The coating further comprises an outer

10 component or module disposed on the inner component formed of ceramic material capable of forming a hydrate or hydroxide compound upon contact with an oxygen containing environment, e.g. water based fluids such as blood, so as to be swellable in such an environment. Preferably, ceramic

15 material for the outer component or module comprises an aluminum, zirconium or hafnium compound, more preferably, a nitride of such materials. The presently most preferred swellable component is a hydrate or hydroxide compound such as aluminum hydroxide, aluminum hydrate, and

mixtures thereof. The inner component is preferably a series of bilayers comprising zirconia and titania and zirconia and alumina. The thicknesses of the coating layers range from about 1 to about 100 nanometers, preferably about 1 to 50 nanometers. The overall coating thickness can range up to  
5 several microns.

Generally, the preferred nanostructure protective coating comprises a plurality of nano-scale inner ceramic layers comprising zirconia, titania, alumina, and an outer nitride based selected from the group consisting of aluminum nitride, zirconium nitride and hafnium nitride.

Furthermore, an implant comprising either or both metallic and  
10 polymeric compounds is provided having the protective coating of the present invention thereon.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

Fig. 1 is a representation of one embodiment of the nanostructure  
15 coating of the present invention.

Fig. 2 . is a representation of idealized changes associated with self-repair in the coating shown in Fig. 1.

Fig. 3 is representation of a Raman spectrum of a single layer nanocrystalline titania.

### **DETAILED DESCRIPTION OF THE INVENTION**

Nanostructured materials have functional units on the order of  $10^{-9}$  meter (m). In other words, the critical morphological features of nanostructures have a dimension approaching atomic distances. The morphology of nanometer-scale (nm) materials gives rise to at least two properties that either alone or in combination can produce ceramics with unique property: (1) a large internal interfacial area exhibiting unique physical and chemical behavior, and (2) the formation of unusual phases in nanocrystallites due to the finite crystal size effect, i.e., a large surface energy contribution to the total Gibbs free energy of formation when the crystallite size is small. The presence of these properties cannot be achieved in traditional ceramics having larger scale microstructures, including low-temperature ductility and superplasticity, high electrical conductivity, thermal shock resistance, enhanced gas sensing, enhanced diffusion barrier action, and enhanced corrosion resistance due to self-sealing behavior.

The protective coatings of the present invention comprise nanostructure coatings, that is coatings having a thickness in a range from about 1 to about 100 nm; preferably from about 1 nm to about 50 nm. The nanostructure coating preferably comprises a plurality of modules comprising  
5 bilayers of different ceramic materials such zirconia, alumina and titania.

A first module comprises a number (m) of zirconia ( $\text{ZrO}_2$ ) and alumina ( $\text{Al}_2\text{O}_3$ ) bilayers; wherein (m) is a number greater than 1. The first module provides toughness to the coating.

A second module disposed on the first module comprises a number (n)  
10 of zirconia ( $\text{ZrO}_2$ ) and titania ( $\text{TiO}_2$ ) bilayers; wherein (n) is a number greater than 1. The second module provides hardness to the coating. Each oxide layer, that is the first and second modules, have a nanoscale lamellar structure, hence, the term nanolaminates.

A third or outer module disposed on the second module comprises a  
15 third-module compound capable of forming a hydrate or hydroxide compound upon contact in an oxygen containing environment, such as blood. The third module preferably comprises an aluminum, zirconium or hafnium compound, more preferably, a nitride of these materials. Module III comprises a single, relatively thicker layer of nanocrystalline aluminum nitride and provides



corrosion resistance to the coating. Corrosion, with its electrochemical nature, is well known to be one of the quintessential issues in thrombus formation. Therefore, a coating whose outermost layer offers *active* corrosion protection is of utmost importance in the material design for the protective coating of the present invention. In general, the driving force for self-sealing is scaled by the decrease in Gibbs free energy that accompanies formation of the reaction product, a surface hydroxide or hydrated oxide. With respect to the ceramics used in the present nanostructure, titania, although widely used as a corrosion-resistant biomaterial because of its chemical inertness, did not self-seal and merely remained unchanged at the blood-coating interface. There was a weak driving force for zirconia and alumina to self-seal in contact with blood, i.e., a decrease in energy of 8.9 kcal/mole for zirconia and 7.8 kcal/mole for alumina. However, the conversion from aluminum nitride to aluminum hydroxide resulted in the much larger energy savings of 370 kcal/mole.

Thus, the coatings of the present invention include one or more layers of nanometer dimensions of zirconia ( $\text{ZrO}_2$ ), titania ( $\text{TiO}_2$ ), alumina ( $\text{Al}_2\text{O}_3$ ), and a nitride such as aluminum nitride (AlN), zirconia nitride and hafnia nitride.

Without limiting the scope of the invention, the following one or more explanations are provided for the mechanism through which the nanostructure coatings of the present invention provide the enhanced performance.

5            Thermodynamic phase evolution of bulk zirconia as it is cooled from the liquid (about 2680°C at atmospheric pressure) is as follows: cubic (about 2360°C) to tetragonal (about 1075°C) to monoclinic (STP phase) Transformation-toughening depends upon retention of tetragonal zirconia at room temperature and local transformation to monoclinic zirconia in response  
10 to stress. The defect structure established within the monoclinic and at the monoclinic/tetragonal boundary toughens the material.

Without limiting the scope of the invention, it is believed that transformation-toughening mechanism works as follows: The stress concentrator at the tip of a growing microcrack triggers a tetragonal-to-  
15 monoclinic zirconia transformation in a small region of material in the crack's path. The daughter monoclinic zirconia has a larger volume than its parent tetragonal zirconia, therefore applying a beneficial compressive stress to the crack tip. The crack tip "blunts" in response to this stress stopping the crack's progress. The cracked material has "repaired" itself by affecting a

transformation of the material at its tip: it has retained its strength and produced toughness on demand.

Without limiting the scope of the invention, the following is believed to be a plausible mechanism by which the nanostructure coatings exhibit “self-sealing” behavior. When a substrate, such as steel, having a microstructure coating comprising nanometer-size crystallites (e.g., aluminum nitride) is exposed to an oxygen containing environment (e.g., water, blood), a chemical reaction occurs converting the surface of nanocrystallite to a hydroxide (e.g., aluminum hydroxide). The conversion results in the “swelling” of the crystallite boundaries. For example, aluminum hydroxide, with a lower density, occupies a larger volume than aluminum nitride. It is further believe, that the hydroxide conversion layer around each crystallite behaves like an atomic level sealant, protecting the underlying structure (e.g., steel) from corrosion. This coating was not an inert or sacrificial coating, rather it changed in a self-limiting, beneficial manner after exposure to a water based electrolyte. Additionally, in a comparison of coatings, it was found that coatings with different crystallite size, nano-crystallinity was advantageous for self-sealing because of the large internal surface area on which a reaction product (e.g., aluminum hydroxide) can form. Specifically,

a decrease in the average crystallite diameter from about 60 to about 10 nm resulted in an order of magnitude decrease in the corrosion rate.

The nanostructure coatings of the present invention are biocompatible material capable of maintaining their integrity over prolonged exposure,

5 making them an ideal coating for metal or polymer implants.

Fig. 1 is a representation of the features of the present invention. In the embodiment, features of which are illustrated in Fig. 1, the nanostructure coating comprises a repeat unit of  $m = 3$  bilayers of zirconia-alumina,  $n = 2$  bilayers of zirconia-titania, and a single layer of nanocrystalline aluminum nitride. The architectural parameters. It should be noted, that a number of factors, alone or in combination, may be varied to achieve nanostructure of the present invention having the desired properties, examples of such factors include: (a) the number ( $m, n$ ) of bilayers in modules I and II, (b) sequencing of all modules, and (c) the thickness of individual oxide layers within each nanolaminate, (d) the thickness of the nanocrystalline aluminum nitride single layer. Furthermore, it should be noted that although a coating may contain hundreds of layers, its functional properties are determined by the structure and interfaces between morphoglogical components within individual layers and the interfaces between layers, that is, at the nanometer level.

Fig. 2 is a representation of the idealized changes associated with self-repair. As can be seen from Fig. 2, (1) some of the tetragonal zirconia crystallites have transformed to monoclinic zirconia in response to mechanical stress in Module I; and (2) a hydroxide layer or skin has formed around the aluminum nitride nanocrystallites in Module III.

### Coating Synthesis

The coatings may be grown by reactive sputter deposition in a radio frequency-excited reactor designed and built for producing ceramic multilayers. An example of such reactor is, a cryogenic pumped, 24" diameter, 304 stainless steel vacuum vessel containing three cathodes excited by three independent generators; a 20" diameter rotating anode;; three quartz crystal thickness monitors; a positive feedback process gas flow system; a substrate (anode) heater; direct current substrate bias capability;; and three viewing ports for optical discharge diagnostics. Preferably, the deposition system is completely programmable and automated, a desirable feature when the growth time of an individual layer in the stack is on the order of a minute. To grow the coatings, substrates are placed on the rotary table covering the anode and moved sequentially under metal targets

covering the cathodes. The targets are sputtered in non-reactive gases such as  $O_2$ ,  $N_2$  in mixtures at a total pressure in the millitorr range. Additionally, stainless steel and fused silica substrates are used, with the deposition proceeding at room temperature. Phase maps for sputter deposited binary oxides and nitrides may be used to guide in the selection of the process parameters.

### **Biocompatibility Evaluation**

The biocompatibility of the coatings may be determined using in vitro optical spectrometric techniques, including infrared (IR) spectroscopy and non-linear Raman microscopy, to image the blood-coating interface. These optical techniques provide information about the local chemistry at the coatings' surface upon exposure to stationary and flowing blood, especially regarding the adsorption of blood plasma proteins, which is related to the surface's hemocompatibility. Standard tests for biocompatibility, including hemolysis and cytotoxicity tests, that measure biocompatibility in terms of changes in a volume of blood in contact with the coating, i.e., "global" tests, may also be utilized. This evaluation approach enables the association of

local changes in chemistry at the blood-coating interface with commonly used benchmarks for noncompatibility obtained from standard global tests.

Optical methods are traditionally used for biomedical diagnostics where there is a need for a non-contact, non-invasive technique to study the interface between two interacting media. Traditionally, IR spectroscopy is used to determine the active vibration modes on the surface of a solid on contact with a liquid. The disadvantage of this technique is obvious when a water-based liquid is used as an interfacing medium: strong IR absorption of water reduces the useful signal and makes accurate measurements extremely difficult. The alternative spectroscopic technique is Raman scattering, which has proved to be effective for non-invasive biomedical diagnostics and blood, as well. The fundamental wavelength of the excitation radiation can be positioned in the non-absorbing region of the spectrum, e.g., at 532 nm or 1064 nm for blood, and the recorded frequency red-shifted scattered radiation contains information about vibrational modes. By confocal imaging of the interface into the detector, a high spatial resolution can be achieved.

The apparatus used for this evaluation, comprises an intracavity doubled neodymium vanadate (Nd:YVO<sub>4</sub>) laser (Millenia V. Spectra-Physics

Lasers, Inc.) delivered through a focusing lens to the sample. Light scattered at 90° is collected by the 200-um diameter multimode fiber, which at the same time, serves as a confocal pinhole and delivery optics to the f/4 imaging spectrometer (TRIAx-320, Instruments Sa). The liquid nitrogen-cooled CCD camera (CCD-2000, Instruments SA, Inc.) has a 1024x256 pixel array chip. The spectrum is dispersed in the horizontal direction, and for an excitation wavelength of 532 nm, covers the range of Raman frequencies from about 110 cm<sup>-1</sup> to 1900 cm<sup>-1</sup>. Spectral resolution is limited by the entrance fiber diameter and the dispersive grating, measured to be 15 cm<sup>-1</sup>. A holographic notch filter (Kaiser Optical Systems, Inc.) is used to improve rejection efficiency, providing six additional orders of magnitude of laser straight light rejection up to about 110 cm<sup>-1</sup> from the 532-nm laser line. The total straight light rejection is estimated be higher than 10 orders of magnitude.

A typical Raman spectrum of a single layer nanocrystalline titania is shown in Fig. 3, The film thickness was about 700 nm, and the substrate was a single crystal silicon from which the native oxide had not been removed prior to deposition. The 520 cm<sup>-1</sup> LO-phonon line of silicon is clearly seen in this spectrum. The 150 cm<sup>-1</sup> and 640 cm<sup>-1</sup> peaks correspond



to the  $E_g$  mode and  $400\text{ cm}^{-1}$  to  $B_{1g}$  mode of anatase phase of titania. The relatively strong line around  $950\text{ cm}^{-1}$  is attributed to silicon-oxygen-titanium bond formation, indicating that there is a strong interaction at the interface between the titania film and the native silicon dioxide layer on the silicon substrate. This latter feature illustrates the sensitivity of Raman spectroscopy to detection of oxide interfaces.

The same type of measurement may be made on the interface of the nanostructured ceramic coatings and blood. These experiments may be done before and after the coating is exposed to blood. Proteins from the blood that are absorbed on the ceramic coating's surface will appear in the Raman spectra. For example, Characteristic peaks corresponding to amid I (about  $1640\text{ cm}^{-1}$ ) and amid II (about  $1540\text{ cm}^{-1}$ ) bands with some modifications due to interaction with ceramic surface are expected appear. The spectroscopic studies may then be compared with the results of the standard biocompatibility tests.

To study the real-time in vitro studies, with the ceramic nanolaminate in direct contact with stationary and flowing blood, Raman spectroscopy may be used. Other parallel methods may also be used to minimize the effect of possible fluorescent background from the blood, for example,

Fourier Transform Raman spectroscopy and nonlinear Raman spectroscopy (Coherent anti-Stokes Raman spectroscopy - CARS). The latter technique has several advantages over traditional Raman spectroscopy, namely: (1) the CARS signal is much stronger when short (picosecond) laser pulses are used; (2) the CARS signal is blue-shifted from the two pump pulses, and thus the fluorescent background may not be a problem; and (3) the CARS signal is highly spatially localized, i.e., it originates only from the focal point of the laser beam, the position at which the laser radiation intensity.

A real-time nonlinear Raman microscope may be used comprising a tunable short pulse laser source, a titanium sapphire amplifier, and an optical parametric amplifier. The detection apparatus comprises the same spectrometer and CCD camera used for the Raman studies, but the holographic notch filter is replaced with a short-wavelength pass filter to select the blue-shifted CARS signal. At least six orders of magnitude improvement in the signal amplitude for the same average laser power, compared to Raman, may be achieved by this technique. Thus, for the same signal-to-noise ratio, several orders of magnitude less pump power is needed, reducing the thermal load and avoiding many unwanted effects associated

with heating. This approach will provide for an instrument for in vitro real-time microscopic diagnostics of biomaterials on the blood interface.

### **Surface Studies**

Scanning electron microscopy (SEM) may be used to study the morphology of the coating surface before and after exposure to blood, including imaging of adsorbates. X-ray photoelectron and Auger spectroscopies may be used for chemical specification and chemical bonding characteristics of the material and any adsorbate present before and after exposure to blood.

### **Electrochemical Corrosion Studies**

Direct current polarization (DC) electrochemical impedance spectroscopy (EIS), and bulk electrolyte pH determination may be carried out on selected nanolaminates on steel substrates. As a reference, bare steel substrates may also be tested. Current-voltage relationships may be obtained from DC measurements under cathodic polarization. The open circuit potential and corrosion current may then be determined from a Tafel plot (cathodic polarization curve) of current-voltage data. EIS may be used to investigate changes in the electrical double layer (EDL) that develops at

the sample's surface when immersed in blood. The capacitance and resistance of the EDL are derived from its chemical composition. Different mechanisms of charge transport through the EDL respond to perturbation at different frequencies. EIS is therefore especially useful for understanding the kinetic process steps associated with corrosion of a ceramic-coated implant by blood. Bulk electrolyte pH values may be determined as a function of exposure time over a period of seven days.

## **EXAMPLES**

### **Example I – Transformation-Toughening Zirconia-Alumina Coatings**

Nanolaminates consisting of polycrystalline zirconia and vitreous alumina bilayer stacks were grown at room temperature by reactive sputter deposition. The formation of tetragonal zirconia in the as-grown material was consistent with a finite crystallite size effect. Solely the tetragonal phase was produced in zirconia layers whose thickness was less than a critical value, e.g., less than 6 nm for room temperature growth. With respect to in-service transformation-toughening, high resolution transmission electron microscopy (HREM) was used to study the post-deposition, stress-

induced tetragonal to monoclinic zirconia transformation, and its plane and direction invariants were identified.

The transformation was localized to nano-sized regions within individual zirconia layers, constrained by the alumina. The macroscopic effect of the toughness resulting from this transformation was confirmed by scanning electron microscopy of a cross-sectioned fracture surface of a nanolaminate growth on a silicon wafer. A crack originating in the silicon wafer was terminated at the wafer-nanolaminate interface, indicating that the nanolaminate had remained intact and adherent to the silicon substrate.

## **Example II – Cubic Zirconia and Zirconia Titanate Formation Zirconia-Titania Nanolaminates at Room Temperature**

As the thickness of each constituent layer in a nanolaminate decreases, the interface between layers plays an increasingly important role in determining the overall properties of the coating. In turn, chemical reactivity between constituents plays an important role in determining the properties of the interface, even at low growth temperature. To illustrate this point, two pseudobinary oxide systems that represented extremes in chemical reactivity between constituents were compared, namely, zirconia-

alumina and zirconia-yttria. The pseudobinary equilibrium phase diagram of zirconia and alumina showed very limited mutual solid solubility and no compounds. On the other hand, the pseudobinary phase diagram of zirconia and yttria showed a series of solid solutions (alloys) covering the entire composition range from pure zirconia to pure yttria, as well as compounds. These two model systems allowed comparison of the effects of chemical reactivity between constituents at their interface in nanolaminates with the same nominal architecture. The results showed that in zirconia-alumina nanolaminates, each binary oxide constituent was a separate entity and their interface was incoherent. In zirconia-yttria nanolaminates, an interfacial reaction between constituents completely obliterated yttria as a separate entity. The reaction product, yttria-stabilized cubic zirconia, grew in the form of needle-like crystallites. These results demonstrated the ability to form interfacial oxide solid solutions at low temperature in a system in which the bulk equilibrium phase diagram predicts reaction between oxide components. Coatings consisting entirely of interface reaction products can therefore be fabricated if the bilayer spacing is small enough.

Thereafter, zirconia-titania nanolaminates were designed having specific phases and interfaces. The bulk zirconia-titania phase diagram

showed three zirconium titanate compounds with closely-related structures:  $\text{ZrTiO}_4$ ,  $\text{ZrTi}_2\text{O}_6$ ,  $\text{Zr}_5\text{Ti}_7\text{O}_{24}$ ; and two alloy phases with limited mutual solid solubility. It was also found that zirconia and titania were reactive during room temperature sputter deposition, with zirconium titanate forming at the bilayer interface. Micron-thick nanolaminates nominally consisting of ultrathin (1.5 nm) zirconia and titania layers actually consisted entirely of their reaction product. Furthermore, the interfacial stress associated with the reaction led to the stabilization of cubic zirconia in nanolaminates with thicker (about 16 to about 22 nm) zirconia layers.

### **Example III – Nanocrystalline Aluminum Nitride for Self-Sealing Corrosion Protection of Steel**

Traditionally, ceramic coatings are used to protect an underlying material from corrosion by providing an inert, non-porous barrier to diffusion. In that case, any defect in the coating, such as a microscopic pore or pinhole, is a possible source of failure due to pitting corrosion. In addition, polycrystalline coatings with a typical columnar crystal structure are intrinsically vulnerable, because this microstructure provides fast diffusion paths to the substrate. To remedy the intrinsic problem of a columnar

microstructure, multilayer coatings may be used to interrupt crystallite growth. However, pitting corrosion due to microscopic defects is still a concern.

The present inventors identified another, active, type of corrosion protection by ceramic coatings, referred to here as "self-sealing" behavior. To develop the self-sealing ceramic coating aluminum nitride coating on steel, as the prototype material, was utilized. The coating microstructure comprised nanometer-size crystallites. When exposed to water, a chemical reaction converted the surface of each nanocrystallite to a hydroxide. The result was that crystallite boundaries "swelled", since aluminum hydroxide, with a lower density, occupied a larger volume than aluminum nitride. The hydroxide conversion layer around each crystallite behaved like an atomic level sealant; protecting the underlying steel from corrosion. The coating was not inert or sacrificial, but changed in a self-limiting, beneficial manner after exposure to the electrolyte. In a comparison of coatings with different crystallite size, nanocrystallinity was an advantage for self-sealing because of the large internal surface area on which a reaction product can form. Specifically, a decrease in the average crystallite diameter from about 60 to



about 10 nm resulted in an order of magnitude decrease in the corrosion rate.

**WHAT IS CLAIMED IS:**

1. A protective coating for an intracorporeal substrate, comprising:
  - a. at least one inner layer formed of ceramic material; and
  - b. an outer layer formed of a water swellable ceramic material.
2. The protective coating of claim 1 including a plurality of inner ceramic bilayers.
3. The protective coating of claim 2 wherein the ceramic material for the inner layers are selected from the group consisting of zirconia, titania and alumina.
4. The protective coating of claim 1 wherein the water swellable ceramic material form a hydrate or hydroxide in the presence of an oxygen containing environment.
5. The protective coating of claim 2 wherein the water swellable ceramic material is selected from the group consisting of alumina, zirconia or hafnia based components.
6. The protective coating of claim 5 wherein the water swellable ceramic material is selected from the group consisting of aluminum nitride, zirconium nitride and hafnium nitride.

7. The protective coating of claim 1 wherein the individual layers are about one to about 100 nanometers thick

8. The protective coating of claim 1 wherein the individual layers are about one to about 50 nanometers thick

9. The protective coating of claim 1 having at least one bilayer of zirconia and alumina.

10. The protective coating of claim 1 having at least one bilayer of zirconia and titania.

11. The coating of Claim 4 wherein the hydrate or hydroxide compound is selected from the group consisting of aluminum hydroxide, aluminum hydrate, and mixtures thereof.

12. The coating of Claim 1 having a thickness of up to about a micron.

13. The coating of Claim 5 wherein the coating has a thickness in a range from about 1 to 50 nanometers.

14. The coating of Claim 1 wherein the first module has a thickness in the range from about 1 to about 100 nm.

15. The coating of Claim 1 wherein the second module has a thickness in the range from about 1 to about 100 nm.

16. The coating of Claim 1 wherein the third module has a thickness in the range from about 1 to about 100 nm.

17. A nanostructure protective coating for a substrate, the coating comprising a plurality of nano-scale ceramic layers comprising at least two components selected from the group consisting of zirconia, titania, alumina, and aluminum nitride.

18. A nanostructure protective coating for a substrate, the coating comprising an outermost coating layer comprising a compound capable of forming a hydrate or hydroxide compound upon contact with an oxygen containing environment and an innermost coating layer comprising a bilayer of ceramic materials.

19. The coating of Claim 18 wherein the outermost layer comprises an aluminum compound.

20. The coating of Claim 19 wherein the aluminum compound is aluminum nitride.

21. An implant, comprising:

a substrate selected from the group consisting of metals, polymers, and a combination thereof; the substrate having a protective coating thereon, the protective coating comprising:

a plurality of modules comprising

a first module comprising a number (m) of bilayers comprising zirconia and alumina wherein (m) is a number greater than 1;

a second module disposed on the first module comprising a number (n) of bilayers comprising zirconia and titania wherein (n) is a number greater than 1; and

a third module disposed on the second module comprising a third-module compound capable of forming a hydrate or hydroxide compound upon contact with an oxygen containing environment.

22. The implant of Claim 21 wherein the third module-compound comprises aluminum.

23. The implant of Claim 21 wherein the third module-compound comprises aluminum nitride.

24. The implant of Claim 21 wherein the hydrate or hydroxide compound is selected from the group consisting of aluminum hydroxide, aluminum hydrate, and mixtures thereof.

25. The implant of Claim 21 wherein the coating is in a range from about 1 to about 100 nanometers.

26. The implant of Claim 21 wherein the coating is in a range from about 1 to 50 nanometers.

27. An intracorporeal implant, comprising:

a substrate selected from the group consisting of metals, polymers, and a combination thereof having a protective coating thereon, comprising:

a plurality of nano-scale ceramic layers of zirconia, titania, alumina, and aluminum nitride.

28. An intracorporeal implant, comprising a substrate selected from the group consisting of metals, polymers, and a combination thereof having a protective coating thereon which has an outermost coating layer comprising a compound capable of forming a hydrate or hydroxide compound upon contact with an oxygen containing environment.

29. The implant of Claim 28 wherein the outermost coating layer comprises an aluminum compound.

30. The implant of Claim 29 wherein the aluminum compound is aluminum nitride.

## **ABSTRACT**

A protective coating for a substrate is disclosed having an outer component or module formed of a swellable material and an inner module formed of a plurality of layer or bilayers formed of ceramic material. The coating comprising a plurality of modules comprising a first module comprising a number (m) of bilayers comprising zirconia and alumina wherein (m ) is a number greater than 1. The coating further comprises a second module disposed on the first module comprising a number (n) of bilayers comprising zirconia and titania wherein (n) is a number greater than 1. The coating further comprises a third module disposed on the second module comprising a third-module compound capable of forming a hydrate or hydroxide compound upon contact with an oxygen containing environment.

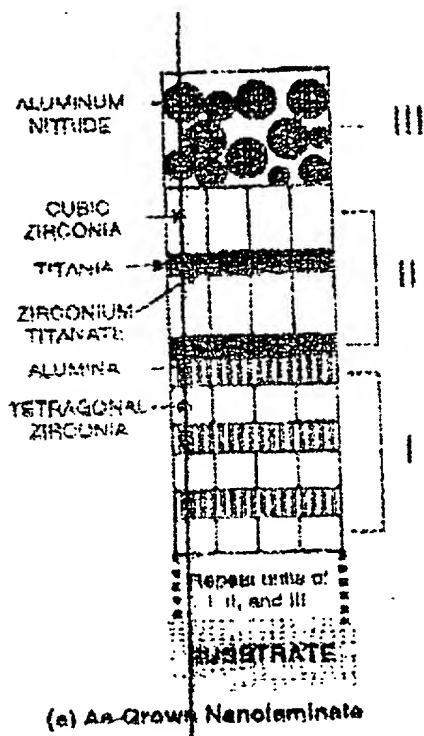


FIG. 1

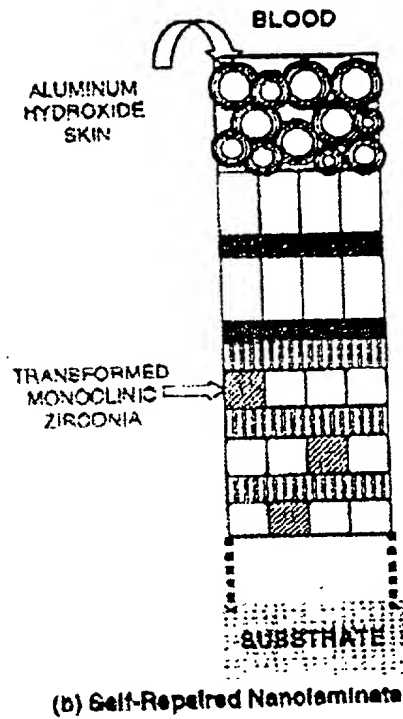


FIG. 2

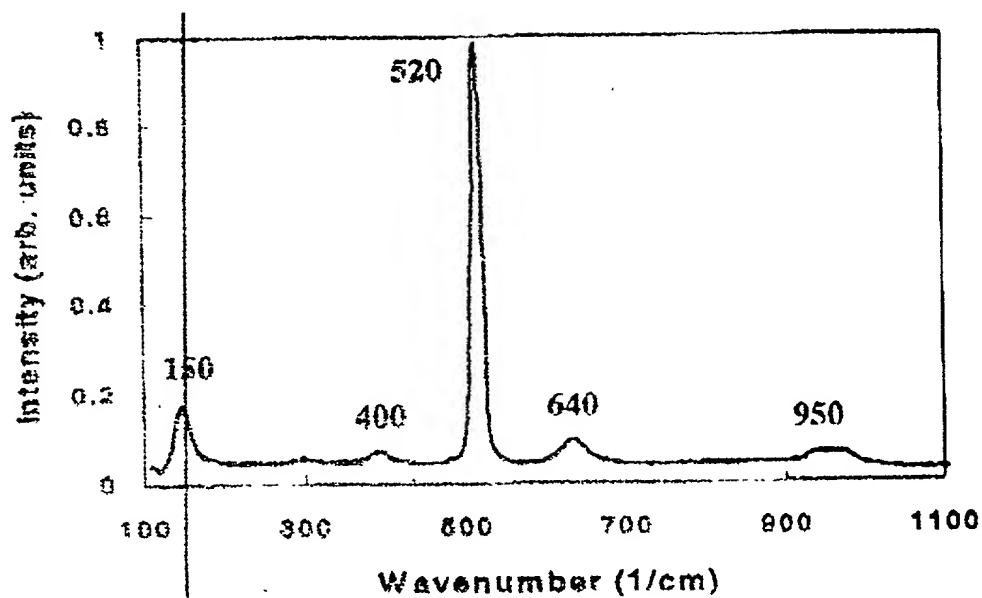


FIG. 3



## DECLARATION AND POWER OF ATTORNEY

As the below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe that I am the original, first inventor of the subject matter which is claimed and for which a patent is sought on the invention entitled **SELF-REPAIRING CERAMIC COATINGS**, the specification of which is attached hereto.

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by or any amendment(s) referred to above.

I acknowledge the duty to disclose information which is material to the examination of this application in accordance with Title 37, Code of Federal Regulations, §1.56(a).

I hereby claim foreign priority benefits under Title 35, United States Code §119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

Prior Foreign Application(s): **NONE**

I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, §1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under §1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

I hereby appoint the following attorneys to prosecute this application and to transact all business in the United States Patent and Trademark Office connected therewith:

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HEWM #3299.01.PA (3MT701!.DOC)